

## Improving Reproducibility in Sputtered Beryllium and Graded Copper Doped Beryllium Capsules

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# Improving Reproducibility in Sputtered Beryllium and Graded Copper Doped Beryllium Capsules

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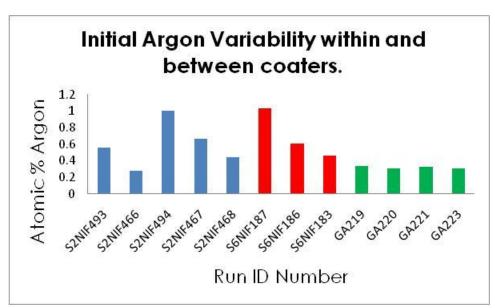
### One of the designs for the NIF ignition targets is a Graded Copper Doped Beryllium Capsule

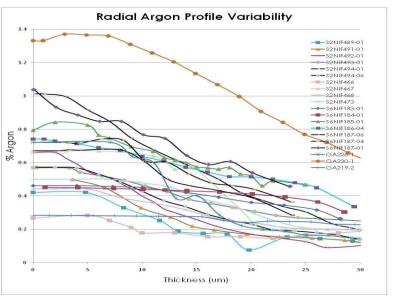
- Several magnetron sputtering systems are dedicated to producing these capsules
  - These systems are located at General Atomics in San Diego and at Lawrence Livermore National Laboratory in Livermore
  - The systems were all assembled at different times with varied gun components, chambers, and configurations
- We needed to minimize the natural variations in coating properties from system to system



### The argon variation within and between the systems needed to be reduced

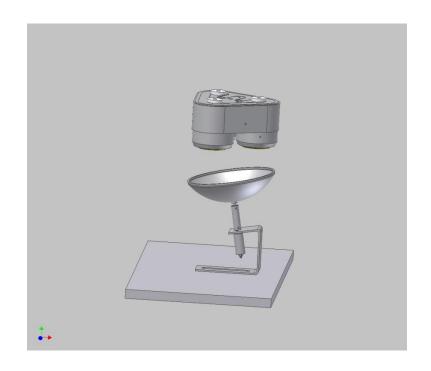
- The atomic percent of argon varied from run to run and from coater to coater
- The radial argon profile also varied





### The coating system with the highest yield of target quality capsules was evaluated

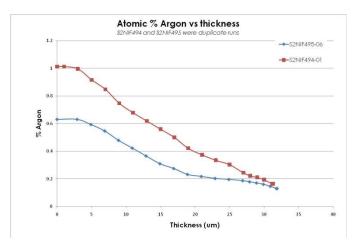
- We wanted to improve the reproducibility of the S2 system and duplicate those results in the other coaters
  - Careful measurements of the system were taken
  - Hard stops and other positioners were designed and installed to decrease run-to-run variability



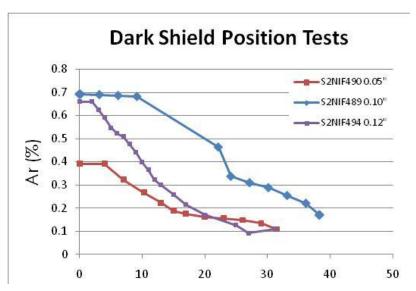
### Even after engineering, argon results were still varied and did not correlate with changes

### We designed a simple experimental matrix

- Changed one parameter slightly (ie, gun to pan distance)
  - Results were not reproducible
  - Trends were not evident



We did not see identical argon results when run conditions were duplicated

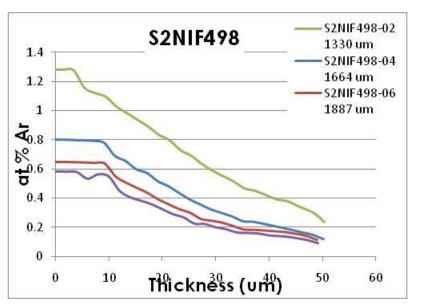


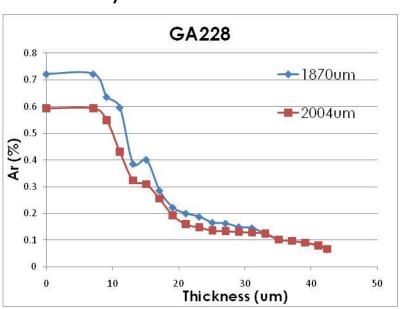
Stepped variations did not indicate any trends



### A run with more than one sized mandrel was completed

- Different profiles were observed and were related to mandrel size
  - This holds true in all 3 coater systems

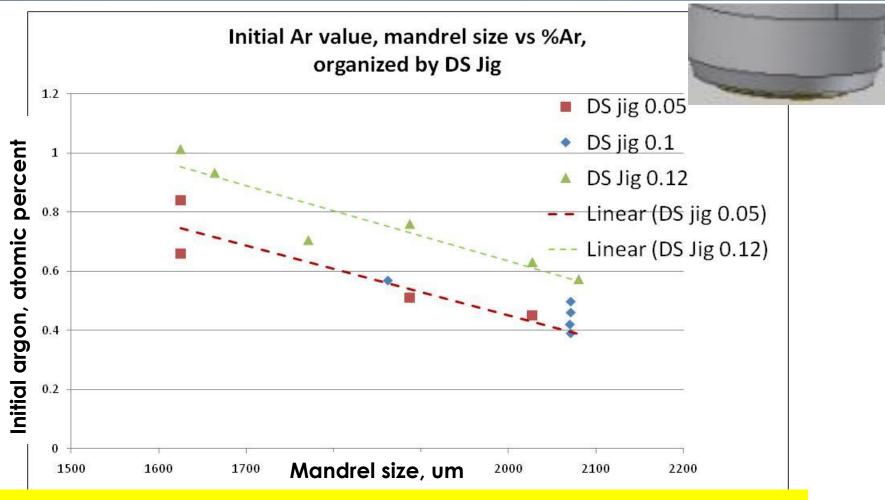




The smaller the mandrel, the higher the initial Argon; but the steady state Ar value stayed the same



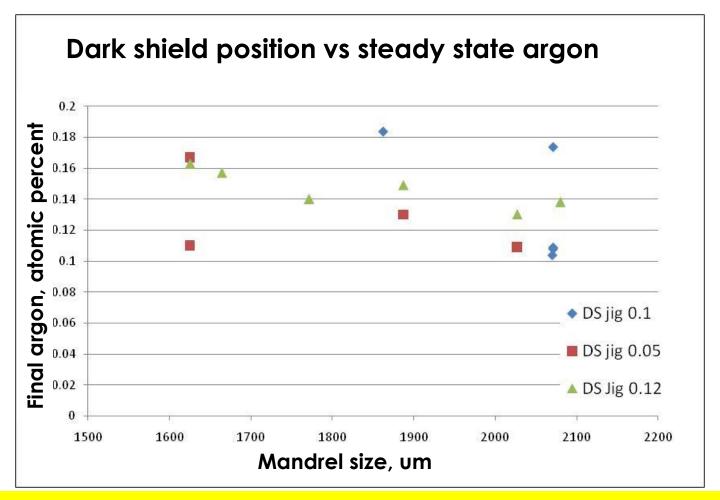
### **Darkshield Position Optimization**



The smallest darkshield-to-target gap results in the lowest initial argon.



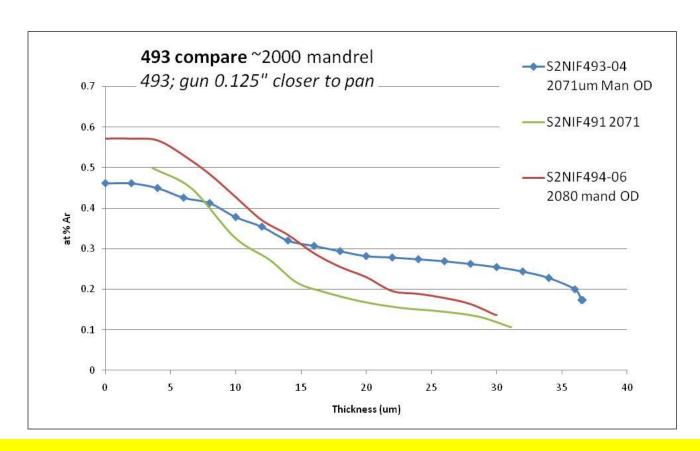
#### **Darkshield Position Optimization**



Final Ar values are not affected by the darkshield position.



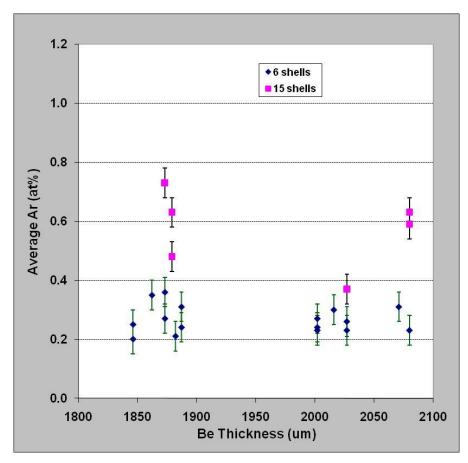
### **Gun-to-pan distance optimization**

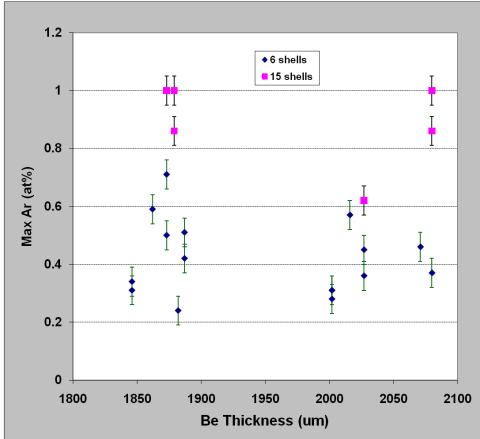


 Steady state argon increased as the distance from the gun to the pan decreased.

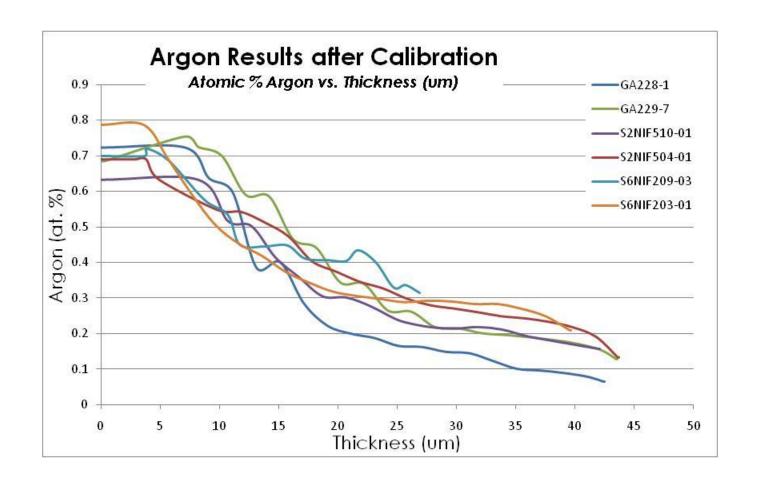


### Increased mandrel quantity increases the Ar concentration

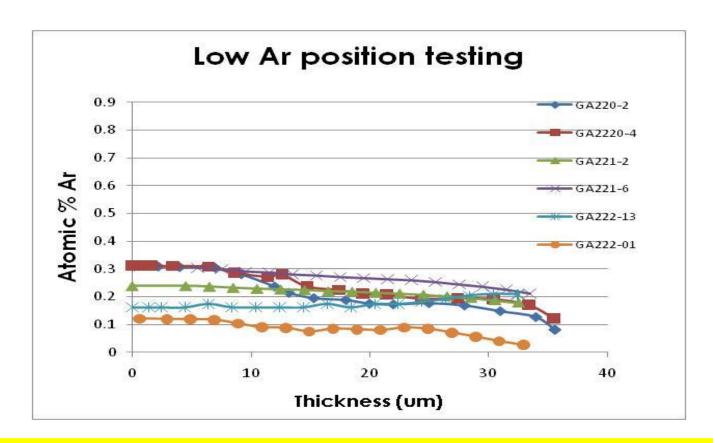




### After careful alignment, argon profiles were reproducible and consistent



### An additional change may result in lower argon

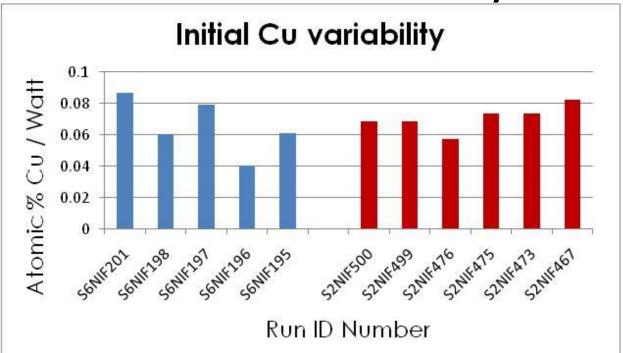


 Lower argon concentration will increase the likelihood of ignition



### The copper coating rate fluctuated

 The point design requirements could not be met without recalibration for every run

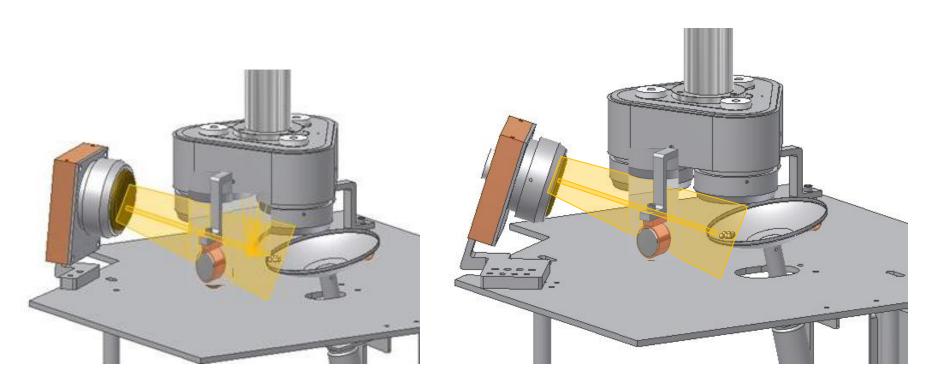


 We needed to optimize our process to improve reproducibility



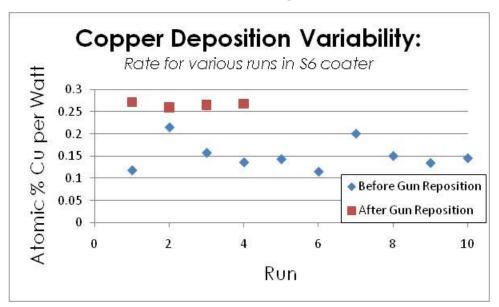
### We optimized the position of the copper gun

The copper gun was repositioned to minimize any shadowing



#### Copper deposition rates stabilized

- Rates were consistent within each coater, but not from coater to coater
  - We were not able to standardize gun position due to chamber configuration restraints



### Coaters all demonstrate nonlinearity between copper wattage and deposition rate

### Expect to see linearity between watts and at % Cu

 Three times the power should equal three times the concentration

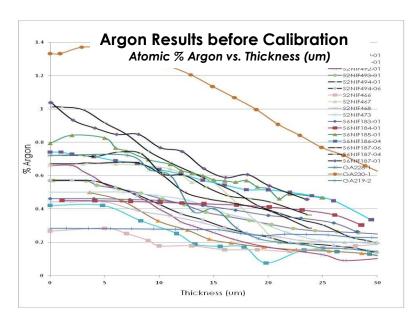
#### All coaters show the same deviation

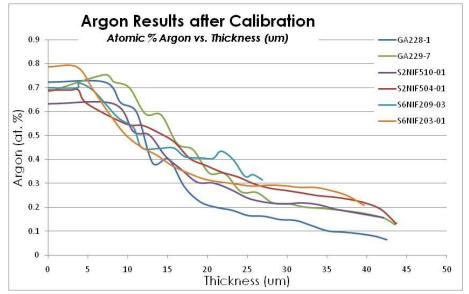
 To increase from 0.5 to 1.5 atomic % Cu, it is necessary to apply 3.6 times more power

Cu Goal	0.5 at %	1.5 at %	
	Watts 1	Watts 2	W2/W1
<b>GA Coater</b>	7.0	25.5	3.64
S2 Coater	2.0	7.3	3.60
S6 Coater	3.4	12.4	3.66

### **Summary of Argon optimization**

 We were able to reduce the run to run and system to system variability of the argon profile with careful calibration of the coating systems





### **Summary of Copper optimization**

 Two of the coaters have been tested and routinely meet specifications

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Date	Run Number	Cu Goal	Cu Actual	In Spec?		
7/17/2009	S2NIF504	0.5	0.51	YES		
7/17/2009	S2NIF504	1.0	1.03	YES		
7/22/2009	S2NIF505	0.5	0.39	YES		
8/4/2009	S2NIF508	0.5	0.5	YES		
8/4/2009	S2NIF508	1.0	1.2	YES		
8/11/2009	S2NIF509	0.5	0.5	YES		
9/2/2009	S2NIF512	0.5	0.5	YES		
9/2/2009	S2NIF512	1.5	1.2	LOW		
9/9/2009	S2NIF513	0.5	0.5	YES		
7/24/2009	S6NIF197	0.5	0.5	YES		
7/24/2009	S6NIF197	1.5	1.39	YES		
7/29/2009	S6NIF198	0.5	0.38	YES		
8/14/2009	S6NIF201	0.5	0.52	YES		
8/14/2009	S6NIF201	1.5	1.36	YES		
8/19/2009	S6NIF202	0.5	0.45	YES		
Break for aperture adjustment						
10/23/2009	S6NIF210	0.6	0.8	YES		
10/23/2009	S6NIF210	1.5	1.6	YES		
10/28/2009	S6NIF211	0.6	0.8	YES		

#### **Further Production Goals**

- We plan to modify the coater configuration to reduce the argon concentration
- We will re-optimize the copper for all systems as we finish the argon modifications